# Memorandum

To: DUNG SY Date: September 12, 2022

Branch Chief, Design M14

North Region Division of Project Development

File: 01-MEN-001-PM 59.8/62.1

EA: 01-0B220 EFIS: 0112000110 Fort Bragg ADA

From: GEOTECHNICAL SERVICES

Office of Geotechnical Design West

Branches A and B

Attention: Ash Arreola

Subject: REVISED GEOTECHNCIAL RECOMMENDATIONS FOR FORT BRAGG ADA

STANDARD RETAINING WALLS

#### Introduction

This Revised Memorandum was prepared in response to the request dated September 9, 2022, for the proposed Fort Bragg ADA project located along State Route (SR) 1 near the intersection with SR 20 in Mendocino County, from PM 59.8 to 62.1. This Memorandum has been revised to update the stationing of Retaining Wall No. 1 and to include recommendations for Retaining Wall No. 2.

The purpose of this memorandum is to provide geotechnical recommendations for the proposed retaining walls. The scope of work included review of pertinent documents, engineering analysis and preparation of this memorandum. No subsurface investigation was performed. The recommendations in this memorandum are based on the Project Plans dated April 12, 2021.

This Memorandum is not intended to be part of the Information Handout and Contract Documents. If needed, a Geotechnical Design Report (GDR) can be prepared for this use.

#### **Project Description**

The Fort Bragg ADA pedestrian infrastructure project consists of the following proposed improvements: replacement and installation of curb ramps, installation of sidewalks, installation of driveways, installation of two retaining walls, and grade corrections by the intersections and crosswalk pavement markings. This memorandum provides geotechnical recommendations for the retaining walls only.

The proposed retaining walls are Standard Retaining Wall, Type 6A. Retaining Wall No. 1 will be parallel to SR 1 in an existing vegetated slope. The slope is approximately 1:1 (H:V)

near the bottom and 3:1 (H:V) near the top. Retaining Wall No. 2 will be parallel to SR 1 in relatively flat terrain. A summary of the proposed retaining wall information is provided in Table 1.

Maximum Location Length Design Retaining **Notes** Height Wall No. (feet) Begin End Line (feet) Station Station 1 RW1 118+18.73 125+58.73 740 6.0 Sloping Backfill 2 RW2 229+98.34 231+86.99 118.65 4.0 Level Backfill

Table 1: Proposed Retaining Wall Summary

#### **Geotechnical Investigation**

No geotechnical investigation was performed for this project.

A 461-foot long Standard Retaining Wall – Type 6 was constructed near the intersection of SR 1 and SR 20 (EA: 01-0A2304). Proposed Retaining Wall No. 1 is a continuation of this existing wall. A subsurface investigation was conducted for the existing wall in August and September 2011. Three hand auger borings and four mud rotary borings were performed. The hand auger borings were advanced to depths of 1.5 to 5.5 feet below ground surface. The mud rotary borings were extended to depths of 15 and 20 feet below ground surface.

The closest geotechnical investigation to Retaining Wall No. 2 was performed for the Pudding Creek Bridge Widening Project (EA 01-43804). Two mud rotary borings were performed in 2016. The closest of the two borings (RC-16-051) is located about 1,000 feet north of proposed Retaining Wall No.1. The boring was advanced to a depth of 105 feet.

A complete description of the subsurface investigations, including the boring locations boring logs, and LOTB are provided in Appendix A.

#### **Geotechnical Conditions**

#### Geology

The project is in the Coast Ranges geomorphic province of California. Both walls are located on the western edge of an uplifted Pleistocene (11,000 to 2,600,000 years old) marine terrace dissected by Pudding Creek to the north and Hare Creek to the south. Approximately 1,500 feet to the west of the site the terrace terminates in an approximately 40-foot high precipitous coastal bluff and to the east a series of older terraces step up into the foothills of the coast range mountains. According to published geologic maps of the area (Jennings 1960, Braun 2005), the site is underlain by rock of the Tertiary to

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Cretaceous, Franciscan Coastal Belt locally overlain by marine terrace deposits. The Coastal Belt Franciscan rock is described as light-colored, well-cemented to deeply weathered, fractured and sheared clastic sedimentary rocks; mostly graywacke sandstone and shale with arkosic sandstone and minor amounts of conglomerate, chert and volcanics. The rock is characterized by coherent and disjointed blocks of various sizes, separated by broad shear zones and faults. The marine terrace deposits are described as consisting of well sorted quartz sand with minor gravel, increasing in age and weathering with increased elevation. There are no known active or potentially active faults within the project limits.

#### Subsurface Conditions

Based on the 2011 investigation for the existing retaining wall near Retaining Wall No. 1, the subsurface soils consist of 6 feet of dune sands underlain by sandstone.

Boring RC-16-051 encountered approximately 9.5 feet of loose clayey sand with gravel interpreted as terrace deposits. Between 9.5 feet and 31.8 feet below ground surface (bgs) (approximate elevations 38.9 to 16.6 NGVD29, feet) the boring encountered dense to very dense, well graded gravel with clay and sand interpreted as decomposed sandstone. Below 31.8 feet the boring encountered rock dominated by sandstone with subordinate argillite which persisted to the depth explored of 105 feet bgs (approximate elevation -56.6 NGVD29, feet).

#### Groundwater

The 2011 subsurface investigation located groundwater at a depth of 9 feet below surface grade, approximately 300 feet from the proposed retaining wall. The same groundwater depth is assumed for Retaining Wall No.1.

Groundwater was measured in RC-16-051 at a depth of 17 feet. The measurement is presumably a partially relaxed groundwater measured between drilling days. The same groundwater depth is assumed for Retaining Wall No. 2.

Groundwater should be expected to vary with time due to seasonal groundwater fluctuations, surface and subsurface flows, ground surface run-off, and other factors that may not be present at the time of the field investigations.

#### Seismic Hazards

#### Site Seismic Parameters

The retaining wall sites may be subject to strong ground motions from nearby earthquake sources during the design life of the walls. The coordinates used in the analysis for Retaining Wall No. 1 and Retaining Wall No. 2 are latitude 39.4209° and longitude -123.8077°, and latitude 39.4508° and longitude -123.8060°, respectively. Based on available subsurface information and SPT correlations for determining shear wave velocity, the time-average shear wave velocity (Vs30) for the upper 100 feet of soil/rock is

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estimated to be 560 m/s (about 1,835 ft/s) for Retaining Wall No. 1 and 390 m/s (about 1,276 ft/s) for Retaining Wall No. 2.

#### **Ground Motion Parameters**

The Design Spectrum for the Safety Evaluation Earthquake, as specified in Caltrans Seismic Design Criteria with October 2019 interim revisions, version 2.0 (SDC v2.0) is the probabilistic response spectrum representing the horizontal ground motion at the site with a 5% probability of exceedance in 50 years (return period = 975 years). The USGS's 2014 NSHM is used as the basis to determine the Design Spectrum in the form of the design Acceleration Response Spectrum (ARS).

Caltrans' web-based tool, ARS online v3.0.2, was utilized to determine the design ground motion parameters, including the ARS, for the subject retaining wall sites. Based on the ARS Online v3.0.2 tool, the design PGA is 0.67g, the deaggregated mean earthquake moment magnitude for PGA, M, is 7.57 and the mean site-to-source distance for 1.0 second period spectral acceleration, R, is 20.8 km (12.9 miles) for Retaining Wall No. 1 and 19.2 km (11.9 miles) for Retaining Wall No. 2.

#### Fault Rupture

The project sites are not located within an Alquist Priolo Earthquake Fault Zone or 1,000 feet from any Holocene or younger aged fault. The nearest active fault is the offshore section of the San Andreas, about 5.8 miles west. There are a series of folds in the marine terraces and one of the folds has been mapped as a compressional fault between Hare Creek and the Noyo River near PM 60.1. This is not an active fault, but rather a mapped remnant of previous tectonic activity. The potential for surface fault rupture does not exist.

#### Liquefaction

Based on the depth of groundwater and the subsurface soil/rock conditions in the nearest borings, the potential for liquefaction does not exist.

#### Recommendations

Proposed Retaining Wall No. 1 is a Standard Plan Retaining Wall, Type 6A (Case 2), with a maximum height of 6 feet. The backfill slope angle should not exceed those shown on the Standard Plans. Proposed Retaining Wall No. 2 is a Standard Plan Retaining Wall, Type 6A (Case 1), with a maximum height of 4 feet.

The footings for Retaining Wall No. 1 will be generally founded in medium dense to dense sands. The factored bearing resistance of the soil will exceed the minimum bearing stresses shown on Standard Plan B3-7B. Since the closest boring to Retaining Wall No. 2 is about 1,000 feet away, the subsurface soils may vary from those disclosed in RC-16-051. The subsurface soils are likely to consist of loose sands. The footing excavation for Retaining Wall No. 2 are to be inspected and approved by the Office of Geotechnical Design West, Branch A. The inspections are to be made after the excavation has been

completed to the bottom of footing elevations and prior to placing concrete or rebar in the excavations. If the subsurface soils are not satisfactory, a minimum of 2-feet of soil below the bottom of footing shall be removed and replaced with angular drain rock. The over-excavation shall extend 2-feet beyond the footing footprint in all directions.

Overall slope stability analyses were performed for Service and Extreme Event Limit States. A horizontal seismic acceleration coefficient of 1/3HPGA (0.22g) was used for the extreme event. Two-dimensional slope stability analyses were performed using the program Slide2 by Rocscience. The factors of safety exceed 1.3 (resistance factor = 0.75) and 1.1 (resistance factor = 0.9) for service and extreme events, respectively.

Standard Plan Earth Retaining Systems (ERS) are designed based on a horizontal seismic acceleration coefficient of 0.2g, corresponding to a HPGA of 0.6g. A Standard Plan ERS can be used in areas with a HPGA greater than 0.6g if the resulting permanent displacement is acceptable for the project. Since the site HPGA is greater than 0.6g, permanent seismic displacement analyses were performed. The Bray et al. (2010) and Bray and Travasarou (2009) methods were used. Based on the analyses, a permanent seismic displacement of 6 inches was estimated.

A Standard Plan Retaining Wall, Type 6A, is acceptable from a geotechnical standpoint if the Designer verifies that 6 inches of permanent seismic displacement is acceptable for the project. In addition, Structure Design should verify the adequacy of the wall design for this site.

As stated earlier, this Memorandum is not intended to be part of the Information Handout and Contract Documents. If needed, a Geotechnical Design Report (GDR) can be prepared for this use

Questions relating to this report should be directed to Nick Briffa at (213) 604-4261 or Branch Chief John Moore at (510) 622-8742.

**NICK BRIFFA** 

Transportation Engineer

Office of Geotechnical Design West

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Branch A

JOHN MOORE

Chief, Branch A

Office of Geotechnical Design West

CHRIS RISK

Chief, Branch

Office of Geotechnical Design West

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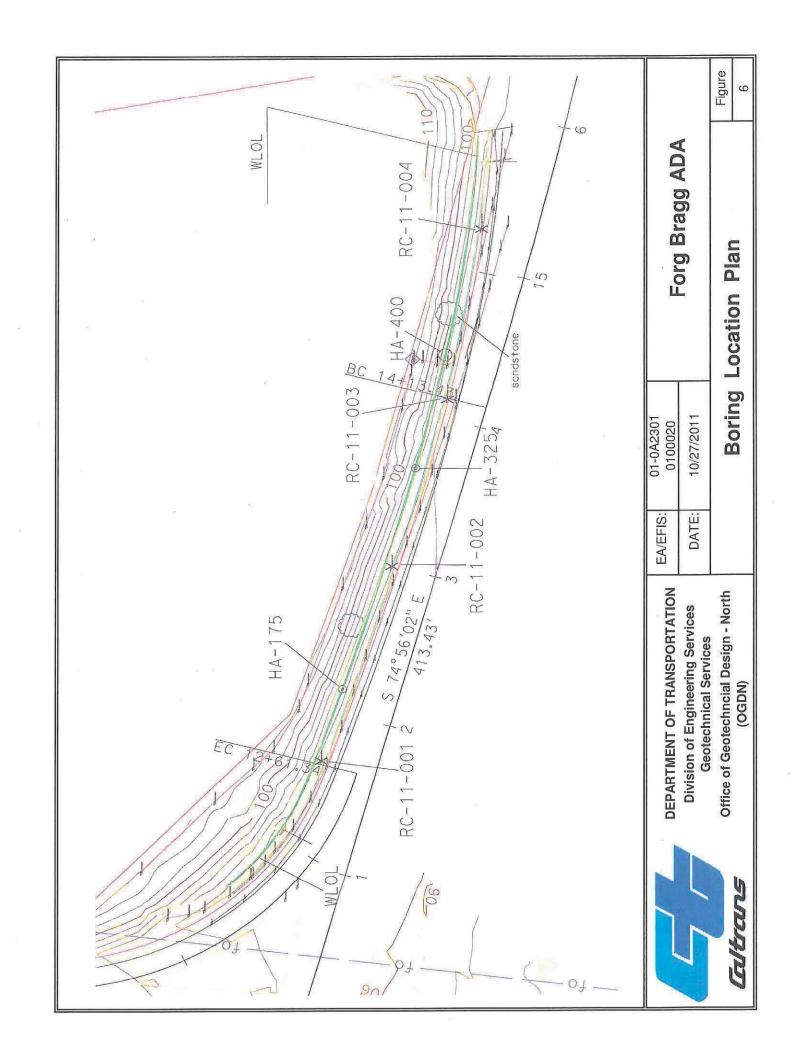
Geotechnical Recommendations Fort Bragg ADA 01-0B220 / 0112000110

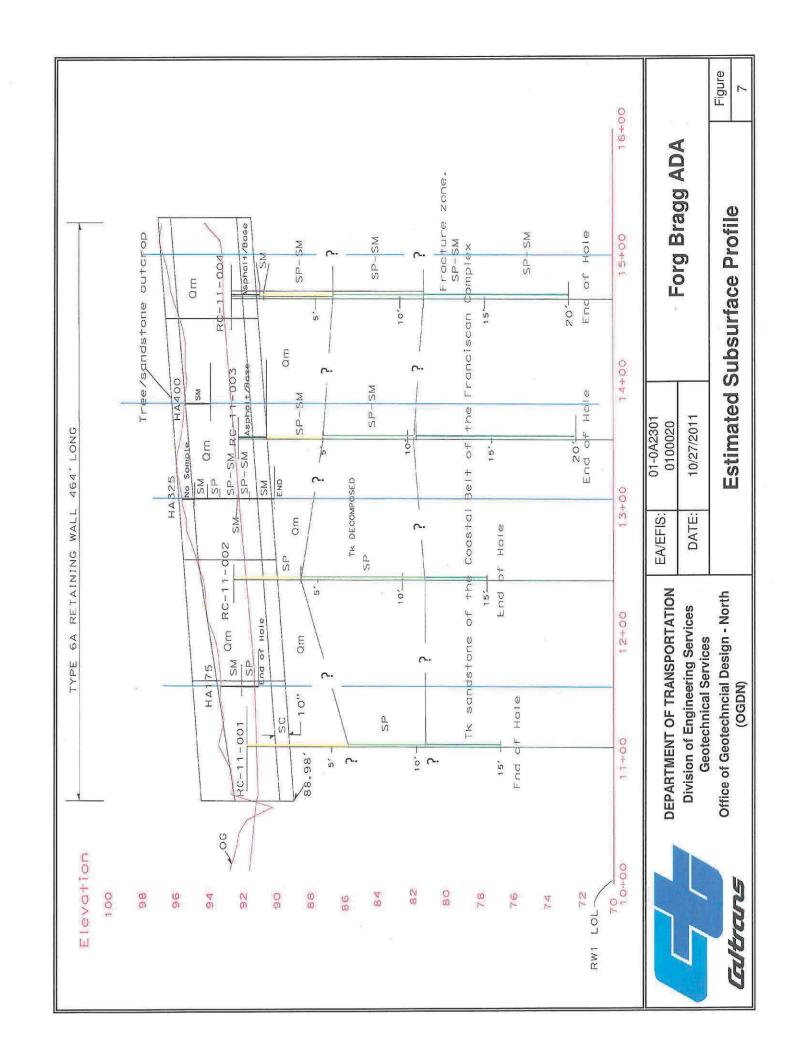
### Attachment

Appendix A Pertinent Subsurface Investigations

c: Robert King, Project Manager, District 3







TL-1271a (REV. 01/31/00)

BORING NUMBER DATE
HA-175 08/25/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)
Wall Station: 11+57

TOP HOLE ELEVATION 92.84'

BOTTOM HOLE ELEVATION

DIST.	CO. MEN	RTE. 20	P.M. (K.P.) R0.0/R0.1	BRIDGE #
BRIDGE OR Fort Brag	R PROJECT NAME g ADA	E	A 01-0A2310//EFI	EA NUMBER S 0100020260
NOTES	0	EQUIPTME	ENT	CHC NUMBER

SUMMARY

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OR		HA-17	5 R	CETIM	002 PF
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			* 1.3	3	-3

GW	DATE
GWS	DATE
CASING SIZE	CASING DEPTH
CASING SIZE	CASING DEPTH
SLURRY TYPE	
SURFACE CONDITION	ONS (Slope, Water, Vegetation, etc)

REMARKS	FI	ELD 1	ESTI	NG		48	DESCRIPTION Soil Classification (group name, group symbol,	
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH (inches) GRAPHIC LOG	GRAPHIC LOG	consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu. Su. Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)	
Hole advanced with a					1			
3.25" sand auger					2			
8					3		Silty SAND (SM); dusky red; dry to moist; mostly fine SAND; little to some fines; few fine	
					5	-	GRAVEL, angular to subangular; weak	
					6		cementation; roots 0-9"	
					7			
	8							
					9		CORN. Laborator de Dintera Antino.	
la l					10		trace coarse to fine GRAVEL, angular;	
					11		beach/dune sand present	
					12		beach/dune sand present	
	-				13	- 1	beach/dune sand present	
al and a second					JANSON TO STATE OF THE PARTY OF	(* 15. 		
					15			
					16	-		
					17		Poorly graded SAND (SP); dry to moist; light	
					18		brownish gray; mostly fine SAND (dune sand) weak cementation	
					19	-	weak comentation	

ORING NUMBER HA-175	08/25/20		DIST. 01					co. MEN	RTE. 20	P.M. (K.P.) R0.0/R0.1	
OCATION (STA/OFFSET or NORTHING/EASTING) 92.84'					OP HC 02.84		EVATI	ATION BRIDGE # EA NUMBEI EA 01-0A2310//EFIS 0100020260			
		FIELD TESTING						DESCRIPTION			
REMARKS (Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)				
						22					
		i i				23			AND with GRAV moist; mostly SA		
						24		coarse, subangu	lar; little to some	GRAVEL.	
						25			ine, includes igne		
						26 27	-	subangular; wea	k cementation.		
						28	Est.				
						29					
						30					
						31					
W						32					
			19		11	33				ž.	
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						50	-				
						51		5			
						53	1				
						54					

TL-1271a (REV. 01/31/00)

AUGER HOLE NUMBER DATE HA-325 08/24/25/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Wall Station: 13+6.28

**BOTTOM HOLE ELEVATION** 

TOP HOLE ELEVATION

95.6

01 MEN BRIDGE OR PROJECT NAME

P.M. (K.P.) RTE. 20 R0.0/R0.1

**EA NUMBER** 

**BRIDGE#** 

EA 01-0A2310//EFIS 0100020260

Fort Bragg ADA CREW

DIST.

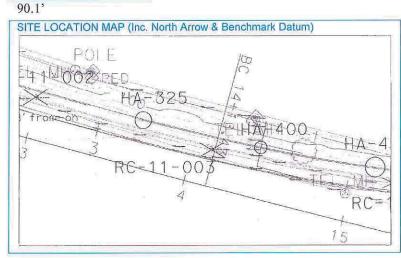
EQUIPTMENT

CHC NUMBER

Beach/dune sand 91' - 93' elevation

CO.

SUMMARY: Beach/dune sand 2.25-4 ft depth; igneous clasts in 48"-60"



DATE
CASING DEPTH
CASING DEPTH

REMARKS (Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions - slowing, chattering, skipping, blocking off)  Hole advanced with a  3.25' sand auger		BLOWS PER 6"	ELEVATION	(leet)	ches	00	Soil Classification (group name, group symbol,
STATE OF THE PRINCIPLE OF	-	B	ELEV	DEPTH (feet)	DEPTH (inches)	GRAPHIC LOG	consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
3.25' sand auger					1		
					2		
					3		
					4		
-					5		0-9" No Samples
					6		, and the second
					7	_	
					8		
#					9		
				4	10		
					11		
94.6' at bottom of this cell			94	1	12		
					13		Silty SAND (SM); pinkish gray; dry; mostly SAND, fine; little to few fines; little to few GRAVEL, fine,
					14		subangular; weak cementation.
				1.25	15		
					16		
					17		
94.1' at bottom of this cell			93.5	1.5	18		
					19		
					20		Poorly graded SAND (SP)

TL-1271b (REV. 01/31/00)

 BORING NUMBER
 DATE
 DIST.
 CO.
 RTE.
 P.M. (K.P.)

 HA-325
 08/24/25/2011
 01
 MEN
 20
 R0.0/R0.1

LOCATION (STA/OFFSET or NORTHING/EASTING)

Wall Station: 13+6.28

TOP HOLE ELEVATION

BRIDGE # EA NUMBER

EA 01-0A2310//EFIS 0100020260

BEMARKS	FI	ELD 1	<b>TESTI</b>	NG			DESCRIPTION
REMARKS (Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	ELEVATION	DEPTH (feet)	DEPTH (inches)	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, q <sub>tt</sub> , s <sub>tt</sub> , Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
					22		
					23		
93.6' at bottom of this cell			93	2	24		Poorly graded SAND (SP); reddish brown; dry; mostly SAND, fine; few GRAVEL, fine, angular to subangular;
					25		weak cementation
					26		Expositional control of the Control of Special Cont
				2.25	27		
					28	7-11	Poorly graded SAND with SILT (SP-SM); dark reddish
					29		brown; moist; mostly SAND, coarse to fine (beach/dune sand included), subrounded to subangular; few to little
93.1' at bottom of this cell 93.1' at bottom of this cell			92.5	2.5	30		GRAVEL, coarse to fine; subangular to angular; weak
					31	1	cementation.
					32		
				2.75			beach/dune sand
			-		33		
			4		34	-	
			92	3	35		,
55.1 de bottom of this con		JE -	72	3	36		
	V				37		
					38		
				3.25	39		Silty SAND with GRAVEL (SM); reddish brown; moist; mostly SAND,
					40		from coarse to fine, angular; little fines; little GRAVEL, coarse to fi
			91.5		41	1.1	angular, intensely weathered rock; weak cementation.
92.1' at bottom of this cell			91.5	3.5	42		
					43		
					44		Poorly graded SAND with SILT (SP-SM); very pale
				3.75	45		brown; moist; mostly SAND, fine, rounded quartz beach/dune sand; few to little fines; trace Gravel, fine (sof
:1					46		clumps of silty sand); weak cementation
					47		
91.6' at bottom of this cell			91	4	48		
					49		
					50		
				4.25	51		Silty SAND (SM); brownish yellow to reddish brown (redder below 48"); moist; mostly SAND, from coarse to
					52		fine; little to some fines, includes coarse white fragments
V					53		of igneous rocks; few-trace GRAVEL, fine, subangular
91.1' at bottom of this cell			90.5	4.5	54		(including hard igneous rocks); weak cementation
				NESS	3.1	1	

TL-1271b (REV. 01/31/00)

BORING NUMBER DATE DIST. CO. RTE. P.M. (K.P.)
HA-325 08/24/25/2011 01 MEN 20 R0.0/R0.1

Wall Station: 13+6.28

TOP HOLE ELEVATION
BRIDGE # EA NUMBER

EA 01-0A2310//EFIS 0100020260

	ELD T	resti	NG			DESCRIPTION		
			_	_	1	DESCRIPTION		
SAMPLE #	BLOWS PER 6"	ELEVATION	DEPTH (feet)	DEPTH (inches)	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)		
				55				
		_		56				
			4,75		-			
						1		
		90	5			few GRAVEL, coarse to fine, angular (very soft sandstor		
	d.					clasts-weathered bedrock?)		
			5.25	63				
				64		increase in fines to "some fines"		
				65				
		89.5	5.5	66				
	,			67	70.5300	End of auger hole at 66"		
				68		1		
+				69				
				******				
				*****				
				77	İ			
				78	1.63			
				79				
				80				
				81				
	*			82				
				83	7	и		
				84				
				85		9		
				86				
		1	1	87	1			
	SAMPLE #	SAMPLE #	SAMPLE	4.75 90 5	S	S		

TL-1271a (REV. 01/31/00)

BORING NUMBER DATE
HA-400 08/24/2011

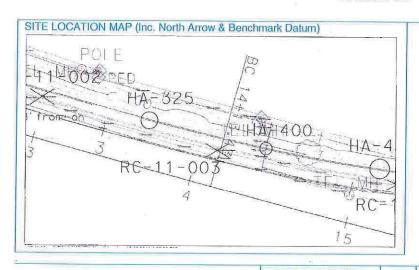
LOCATION (STA/OFFSET or NORTHING/EASTING)

Wall Station: 13+82

TOP HOLE ELEVATION 95.43

DIST.	CO.	RTE.	P.M. (K.P.)	BRIDGE #
01	MEN	20	R0.0/R0.1	
BRIDGE OF	R PROJECT NAME			EA NUMBER
E D	g ADA	E	A 01-0A2310//EFIS	\$ 0100020
Fort Brag	8		TOT OF THE TOTAL I	0.000=0

HAMMER ID#



aw .	DATE
GWS	DATE
CASING SIZE	CASING DEPTH
CASING SIZE	CASING DEPTH
SLURRY TYPE	

REMARKS	FI	ELD T	ESTI	NG			DESCRIPTION
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
Hole advanced with a					1		Silty SAND with GRAVEL (SM); loose;
3.25" sand auger					2		brownish yellow; moist; mostly SAND, fine;
					3		little fines; little fine to coarse GRAVEL;
					4		subangular. Gravel consists of soft fragments of intensely weathered fine sandstone.
2					5		intensery weathered line sandstone.
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					7	111	8
					8		
					9	- [1]	ė.
					10		a
					11		2
					12		
					13		
					14		
		- 55			15	-15	
					16	捌	
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					18		
					19		
_					20		
				10	21		

TL-1271a (REV. 01/31/00) BORING NUMBER DATE 09/07/2011 RC-11-001

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 11+67, 31 L

TOP HOLE ELEVATION

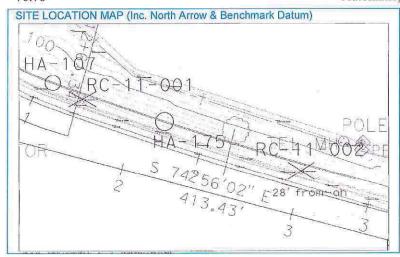
91.78

**BOTTOM HOLE ELEVATION** 

76.78

DIST.	CO.	RTE.	P.M. (K.P.)				
01	MEN	20	R0.0/R0.1				
PROJECT				EA NUMBER			
Fort Brag	g ADA	_ E	EA 01-0A2310//EFIS 01000				
CREW		EQUIPTME	NT	CHC NUMBER			
Eureka Drill Crew		Acker		1974			
HAMMER							

Automatic, ER=80% (Calibrated 04/19/2011)



COLAT	
GW	DATE
CASING SIZE	CASING DEPTH
94 mm	10'
CASING SIZE	CASING DEPTH
SLURRY TYPE	
None	Drilled with Water
PLIDENCE CONDITIONS	(Slope, Water, Vegetation, etc)

TALLY CONTROL OF TAXABLE PARTY.						10		
REMARKS	F	IELD 7	TEST	ING		O	DESCRIPTION	
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition – Caving, Squeezing, Loss of Circulation, etc.  Drill Rig reactions – slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor other characteristics)	
Mud rotary punch core, 4.75" finger bit		4			1.		Clayey SAND (SC); medium dense; reddish brown;	
to 10.6'. Drilled dry to 2'.		5			2		moist; mostly SAND, fine; little fines; weak cementation to 3". [Qm]	
Corrected N: 13 x 1.33=17.3, medium dense		8	13	79	3		moderate cementation from 3'to 5'	
а					4		brownish yellow from 3' to 7'.	
					5		C. C	
Corrected N: 22 x 1.33=29, medium dense		18			6		fewer fines; weak cementation; becoming decomposed sandstone	
W		9			7		SEDIMENTARY ROCK (Sandstone); brownish yellow;	
		13	22		8		intensely weathered to decomposed; (Poorly graded SAND (SP); medium dense; moist; mostly SAND, from coarse to	
			9 fine; little fines; fe	fine; little fines; few GRAVEL, from coarse to fine, angula				
78					10		weak cementation). [DECOMPOSED BEDROCK, Tk]	
Refusal at 10.6' 81.1' elevation)		41			11		SEDIMENTARY ROCK (Sandstone); massive; yellowish	
3 ¾"diamond core bit from 10.6' to 15'.		65/1.5	R		12		brown; intensely weathered; moderately hard; very intensel	
	4				13		fractured. [BEDROCK, Tk]	
					14			
End of hole at 15' (Elevation 76.78').					15			
Perforated 0- 10'. Bentonite below 10'.					16			
One bag of sand					17			
					18			
-					19	-		
					20			
	1	1			60.00			

TL-1271a (REV. 01/31/00)
BORING NUMBER
RC-11-002

DATE 09/07/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 13+00, 25.3 L

TOP HOLE ELEVATION

92.54

BOTTOM HOLE ELEVATION 77.54'

DIST.

CO. MEN RTE. 20 P.M. (K.P.) R0.0/R0.1

PROJECT

Fort Bragg ADA

EA 01-0A2310//EFIS 0100020260

CREW

Eureka Drill Crew

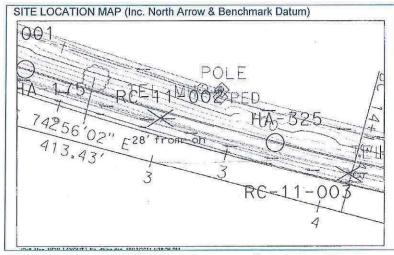
N

EQUIPTMENT Acker CHC NUMBER 1974

**EA NUMBER** 

HAMMER

Automatic, ER=80% (Calibrated 04/19/2011)



LOGGER  D. McGuire	=
SW	DATE
9.3' bgs	9/8/2011
<b>GW</b>	DATE
CASING SIZE	CASING DEPTH
94 mm	15'
CASING SIZE	CASING DEPTH
SLURRY TYPE	
Vone	Drilled with Water
	ONS (Slope, Water, Vegetation, etc)
	g bank, surface dry, drilled into soil at to edge of pavement,

TOWN MAN NICH LAYOUT I NO MENS AND TOUR PORT LIBERS OUT		7							
REMARKS	FIELD	TEST	TING		က္ဆ	DESCRIPTION			
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc.  Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE # BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, Su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor other characteristics)			
Mud rotary punch core, 4.5" finger bit to	4			1		Poorly graded SAND (SP); dense; reddish brown; moist; mostly			
10.75'. Drilled dry to 2'.	6			2		SAND, fine to coarse; little fines; weak cementation to (0" to 6")			
Corrected N: 27x 1.33=36 (dense due to	21	27		3		Brownish yellow; trace to few GRAVEL, coarse; subangular (6 1.5').			
a fragment of coarse gravel)				4		1.5 ).			
200 200 01 00000 00	8			5		Poorly graded SAND with SILT and GRAVEL (SP-SM); dense to medium dense; brownish yellow; moist; mostly SAND, from			
Corrected N: 19x 1.33=25.3 (medium	13			6	11:13	coarse to fine; little GRAVEL, fine, from angular to subrounded;			
dense)	7			7		cementation from weak to moderate (1.5'-5').			
	12	19		8		SEDIMENTADA DOCK (Conditional), buquinish vellanii interes			
				9		SEDIMENTARY ROCK (Sandstone); brownish yellow; intensely weathered to decomposed; (Poorly graded SAND (SP); medium			
				10		dense; moist; mostly SAND, fine; little fines; moderate cementation). [DECOMPOSED BEDROCK, Tk]			
Refusal at 11.3' (81.24')	14			11		cementation). [DECOMPOSED BEDROCK, 1k]			
3 ¾"diamond core bit from 11.3' to 15'.	50/5	5		12					
	50/3	5 100/9		13		SEDIMENTARY ROCK (Sandstone); massive; dark grayish brown; intensely weathered; moderately hard; very intensely			
				14		fractured. [BEDROCK, Tk]			
End of hole at 15' (77.54' elevation).				15					
Casing perforated 5' to 15'.				16					
Two bags of sand and bentonite.				17					
7 39 .	1			18					
				19		9			
				20					

TL-1271a (REV. 01/31/00)

BORING NUMBER DATE RC-11-003 09/08/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 14+13, 23 L;

TOP HOLE ELEVATION

92.24

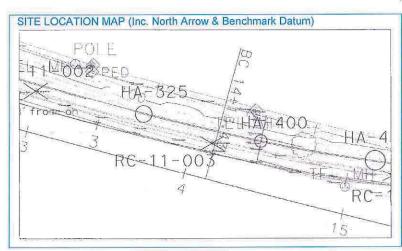
**BOTTOM HOLE ELEVATION** 

72.24

DIST.	CO.	RTE.	P.M. (K.P.)				
01	MEN	20	R0.0/R0.1				
PROJECT Fort Brag	α A D A	EA 01-0A2310//EFIS 0100020260					
CREW	g ADA	EQUIPTME	AN AUTHORNOOM AND THE AND				
Eureka Drill Crew		Acker	1974				

HAMMER

Automatic, ER=80% (Calibrated on 04/19/2011)



SW/	DATE
·W	DATE
ASING SIZE	CASING DEPTH
4 mm	20'
ASING SIZE	CASING DEPTH
LURRY TYPE	
lone	Drilled with Water

REMARKS	F	FIELD	TESTI	NG.		90	D
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc.  Drill Rig reactions - slowing, chattering, skipping blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	S de CR
Mud rotary punch core, 4 ¾" finger bit					1		2
to 10.5'. Dry SPT 0-1.5'.					2		
		12			3		
		27			4		
18"-36" very dense, N>50		31	58		5		
El .		33			6		
Very dense, N>50		60/6			7		
		29	89/12		8		
					9		1
					10		3
Refusal at 10.5' (81.74' elevation).		50/5.5	R		11		
3 ¾"diamond core bit from 10.5' to 20'.					12		
					13		- 1
1.65					14		- *
я					15		
					16		
					17		
End of hole at 20' (elevation 72.24')					18		
Casing perforated 10' to 20'.					19		
Two bags of sand; bentonite to seal hole.					20		1000

#### DESCRIPTION

Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, q<sub>u</sub>, s<sub>u</sub>, Other characteristics)

Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)

ASPHALT and road base.

Poorly graded SAND with SILT (SP-SM); very dense; brownish yellow to yellowish red; moist; mostly SAND, fine; few to little fines; from moderate to weak cementation. [Qm]

SEDIMENTARY ROCK (Sandstone); brownish yellow; very intensely weathered to decomposed; (Poorly graded SAND with SILT and GRAVEL (SP-SM); very dense; moist; mostly SAND, fine; few to little fines; from moderate to weak cementation.). [DECOMPOSED BEDROCK, Tk]

SEDIMENTARY ROCK (fine-grained Sandstone); massive; reddish brown; intensely weathered; moderately soft; very intensely fractured; fracture zone. [BEDROCK, Tk]

TL-1271a (REV. 01/31/00) BORING NUMBER DATE 09/08/2011 RC-11-004

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 15+25, 31.3 L

Two bags of sand; bentonite plug).

TOP HOLE ELEVATION

92.64

**BOTTOM HOLE ELEVATION** 

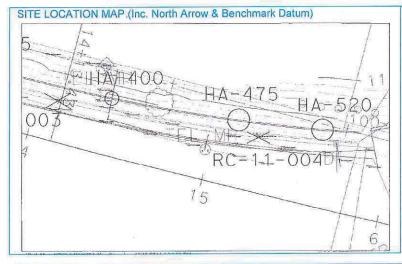
72.64

DIST.	CO.	RTE.	P.M. (K.P.)			
01	MEN	20	R0.0/R0.1			
PROJECT				EA NUMBER		
Fort Brag	g ADA	E	EA 01-0A2310//EFIS 01000202			
CREW		EQUIPTME	NT	CHC NUMBER		
Eureka Di	rill Crew	Acker		1974		

Automatic, ER=80% (Calibrated 04/19/2011)

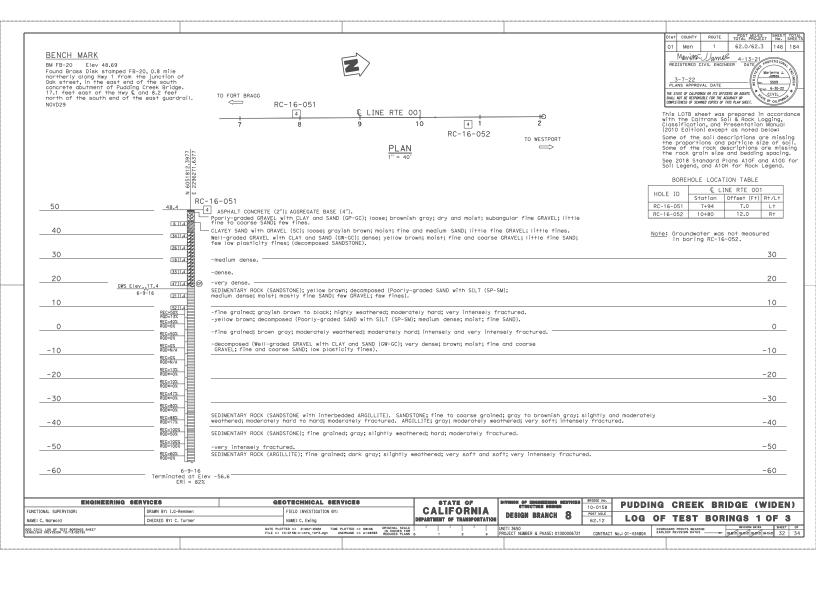
N

HAMMER



W	DATE
SW.	DATE
ASING SIZE	CASING DEPTH
4 mm	20'
ASING SIZE	CASING DEPTH
LURRY TYPE	
lone	Drilled with Water
	ONS (Slope, Water, Vegetation, etc)
nny, dry paveme	Control of the Contro

TO THE LITTLE WHITE WAY IN AN AND AND AND AND AND AND AND AND AND				1						
REMARKS (Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc.  Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6" TI	SPT (N) TAS	Recovery % S	ОЕРТН	GRAPHIC LOG	DESCRIPTION Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics) Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)			
Mud rotary punch core; 4 3/4" finger bit.					1		ASPHALT and road base.			
		10			2		Poorly graded SAND with SILT (SP-SM); medium dense; reddish			
Corrected N (20"-38"): 15x 1.33=20		7			3		brown; moist; mostly SAND, fine; few to little fines; moderate cementation (1.7'-4.3') [Qm]			
Medium dense		8	15							
					5		very dense; brownish yellow; few to little GRAVEL, from coar to fine; (4.3'-5.3'). [Qm]			
		13			6					
Very dense, N>50		20			7		SEDIMENTARY ROCK (Sandstone); reddish brown; intensely			
		37	57		8		weathered to decomposed; (Poorly graded SAND with SILT (SP-SM); very dense; moist; mostly SAND, fine; few to little fines;			
					9		moderate cementation. (5.3'-11.4'). [DECOMPOSED			
					10		BEDROCK, Tk]			
Refusal at 11.4' (81.2' elevation)		22			11					
3 3/4" diamond core bit from 11.4' to 20'.	a a	37			12		SEDIMENTARY ROCK (Sandstone); reddish brown; intensely			
		60/5	97/11		13		weathered to decomposed; (Poorly graded SAND with SILT (SP-SM); very dense; moist; mostly SAND, mostly fine but includes			
					14		coarse; few to little fines; moderate cementation) [BEDROCK,			
					15		Tk].			
18' drill rate increased through soft material					16					
and black organic film appeared in mud pit.					17		fracture zone 18'-20'.			
End of hole at 20' (elevation 72.64).					18		Andread State Control of the Control			
Casing perforated 10' to 20'.					19		gray at 19'-20'.			



# Memorandum

To: DUNG SY Date: October 31, 2022

Design M14

Attention: Ash Arreola

North Region Division of Project Development

File: 01-MEN-001-PM 59.8/62.1

EA: 01-0B220 EFIS: 0112000110 Fort Bragg ADA Retaining Wall – 1N

Retaining Wall - 2S

From: GEOTECHNICAL SERVICES

Office of Geotechnical Design - West

Branches A and B

Subject: GEOTECHNICAL DESIGN REPORT FOR FORT BRAGG ADA RW-1N and RW-2S

#### Introduction

This Geotechnical Design Report (GDR) was prepared in response to the request dated September 9, 2022, for the proposed Fort Bragg Americans with Disabilities Act (ADA) project located along State Route (SR) 1 in Mendocino County, from PM 59.8 to 62.1. The purpose of this report is to provide geotechnical recommendations for the proposed retaining walls. The recommendations in this memorandum are based on the Project Plans dated April 12, 2021. The scope of work included review of pertinent documents, engineering analysis and preparation of this memorandum. No subsurface investigation was performed.

#### **Project Description**

The Fort Bragg ADA pedestrian infrastructure project consists of the following proposed improvements: replacement and installation of curb ramps, installation of sidewalks, installation of driveways, installation of two retaining walls, and grade corrections by the intersections and crosswalk pavement markings. This memorandum provides geotechnical recommendations for the retaining walls only.

Retaining Wall No. 1 (RW-1N) is a Standard Retaining Wall, Type 6A, and will be constructed parallel to SR 1 in an existing vegetated slope. The slope is approximately 1H:1V near the bottom and 3H:1V near the top. Retaining Wall No. 2 (RW-2S) is a Standard Retaining Wall, Type 6B, and will be constructed parallel to SR 1 in relatively flat terrain. A summary of the proposed retaining wall information is provided in Table 1 and the locations of the walls are shown in Figure 1, Site Vicinity Map.

All elevations referenced in this report are based on the North American Vertical Datum of 1988 (NAVD88), unless otherwise noted.

Table 1: Proposed Retaining Wall Summary

Retaining	Wall		Location		Length	Maximum Design	Notes	
Wall			End Station	(feet)	Height (feet)	Notes		
RW-1N	Type 6A Case 2	RW1	118+18.73	125+58.73	740	6.0	Sloping Backfill	
RW-2S	Type 6B Case 1	RW2	229+98.34	231+86.99	188.65	4.0	Level Backfill	

#### **Geotechnical Investigation**

No subsurface exploration or laboratory tests were performed for this project.

A 461-foot long Standard Retaining Wall – Type 6 was constructed near the intersection of SR 1 and SR 20 (EA: 01-0A2304). Proposed RW-1N is a continuation of this existing wall. A subsurface investigation was conducted for the existing wall in August and September 2011. Three hand auger borings and four mud rotary borings were performed. The hand auger borings were advanced to depths of 1.5 to 5.5 feet below ground surface (EI. 93.9 to 90.1 feet). The mud rotary borings were extended to depths of 15 and 20 feet below ground surface (EI. 76.8 to 72.2 feet).

The closest geotechnical investigation to RW-2S was performed for the Pudding Creek Bridge Widening Project (EA 01-43804, Bridge No. 10-0158). Two mud rotary borings were performed in 2016. The closest of the two borings (RC-16-051) is located about 1,000 feet north of proposed RW-2S. The boring was advanced to a depth of 105 feet (EI. -56.6 feet).

A complete description of the subsurface investigations, including the boring locations boring logs, and LOTB are provided in Appendix A.

#### **Geotechnical Conditions**

#### Geology

The project is in the Coast Ranges geomorphic province of California. Both walls are located on the western edge of an uplifted Pleistocene (11,000 to 2,600,000 years old) marine terrace dissected by Pudding Creek to the north and Hare Creek to the south. Approximately 1,500 feet to the west of the site the terrace terminates in an approximately 40-foot high precipitous coastal bluff and to the east a series of older terraces step up into the foothills of the coast range mountains. According to published geologic maps of the area (Jennings 1960, Braun 2005), the site is underlain by rock of the Tertiary to Cretaceous, Franciscan Coastal Belt locally overlain by marine terrace deposits. The Coastal Belt Franciscan rock is described as light-colored, well-cemented to deeply

DUNG SY October 31, 2022 Page 3 Geotechnical Design Report Fort Bragg ADA RW-1N and RW-2S 01-0B220 / 0112000110

weathered, fractured and sheared clastic sedimentary rocks; mostly graywacke sandstone and shale with arkosic sandstone and minor amounts of conglomerate, chert and volcanics. The rock is characterized by coherent and disjointed blocks of various sizes, separated by broad shear zones and faults. The marine terrace deposits are described as consisting of well sorted quartz sand with minor gravel, increasing in age and weathering with increased elevation. There are no known active or potentially active faults within the project limits.

#### **Surface Conditions**

The retaining wall locations are located near the Pacific Coast on SR 1 where the Noyo River and Pudding Creek flow into the Pacific Ocean. Pavement elevations near RW-1N on the existing highway range from 91 feet to 112 feet, south to north, respectively. Existing cut and natural slopes in the vicinity range from 1H:1V to 3H:1V. Upslope of proposed RW-1N is a shopping center.

Near RW-2S, the ground surface is relatively flat with a pavement elevation of about 64 feet to 65 feet. Proposed RW-2S is adjacent to a vacant lot.

#### **Subsurface Conditions**

Based on the 2011 investigation for the existing retaining wall near RW-1N, the subsurface soils consist of 6 feet of dune sands underlain by sandstone.

For RW-2S, Boring RC-16-051 encountered approximately 9.5 feet of loose clayey sand with gravel interpreted as terrace deposits. Between 9.5 feet and 31.8 feet below ground surface (bgs) (approximate elevations 38.9 to 16.6 NGVD29, feet) the boring encountered dense to very dense, well graded gravel with clay and sand interpreted as decomposed sandstone. Below 31.8 feet the boring encountered rock dominated by sandstone with subordinate argillite which persisted to the exploration depth of 105 feet bgs (approximate elevation -56.6 NGVD29, feet).

#### Groundwater

The 2011 subsurface investigation located groundwater in boring RC-11-002 on September 8, 2011, at a depth of 9.3 feet below surface grade (El. 83.2 feet), approximately 300 feet from the proposed retaining wall. The same groundwater depth is assumed for RW-1N.

Groundwater was measured in RC-16-051 on June 9, 2016, at a depth of 31 feet (El. 17.4 feet). The measurement is presumably a partially relaxed groundwater measured between drilling days. The same groundwater depth is assumed for RW-2S.

Groundwater should be expected to vary with time due to seasonal groundwater fluctuations, surface and subsurface flows, ground surface run-off, and other factors that may not have been present at the time of the field investigations.

#### Seismic Hazards

#### Site Seismic Parameters

The retaining wall sites may be subject to strong ground motions from nearby earthquake sources during the design life of the walls. The coordinates used in the analysis for RW-1N and RW-2S are latitude 39.4209° and longitude -123.8077°, and latitude 39.4508° and longitude -123.8060°, respectively. Based on available subsurface information and SPT correlations for determining shear wave velocity, the time-average shear wave velocity (Vs30) for the upper 100 feet of soil/rock is estimated to be 560 m/s (about 1,835 ft/s) for RW-1N and 350 m/s (about 1,148 ft/s) for RW-2S.

#### **Ground Motion Parameters**

The Design Spectrum for the Safety Evaluation Earthquake, as specified in Caltrans Seismic Design Criteria with October 2019 interim revisions, version 2.0 (SDC v2.0) is the probabilistic response spectrum representing the horizontal ground motion at the site with a 5% probability of exceedance in 50 years (return period = 975 years). The USGS's 2014 National Seismic Hazard Model (NSHM) is used as the basis to determine the Design Spectrum in the form of the design Acceleration Response Spectrum (ARS).

Caltrans' web-based tool, ARS online v3.0.2, was utilized to determine the design ground motion parameters, including the ARS, for the subject retaining wall sites. Ground motion parameters are summarized in Table 2.

Table 2: Recommended Ground Motion Parameter for Geotechnical Design

	Sit	e Parameters		Design Gro	und Motion Pa	rameters		
				(Return Period = 975 Years)				
Project Component ID	Latitude (degrees)	Longitude (degrees)	Shear Wave Velocity (V <sub>S30</sub> ) (m/s)		Mean Earthquake <sup>(1)</sup> Moment Magnitude (M)	Mean Site- to-Fault Source Distance (1) (R) (km)		
RW-1N	39.4209°	-123.8077°	560	0.65	7.57	20.8		
RW-2S	39.4508°	-123.8060°	350	0.67	7.58	21.3		

<sup>1.</sup> Based on Caltrans web tool ARS Online (Version 3.0.2)

#### Parameters for Seismic Slope Stability Analysis

A horizontal seismic coefficient (k<sub>h</sub>) of 0.22g, equal to 1/3 HPGA, is used for seismic slope stability analyses of the retaining walls.

DUNG SY October 31, 2022 Page 5 Geotechnical Design Report Fort Bragg ADA RW-1N and RW-2S 01-0B220 / 0112000110

#### Fault Rupture

The project sites are not located within an Alquist Priolo Earthquake Fault Zone or 1,000 feet from any Holocene or younger aged fault. The nearest active fault is the offshore section of the San Andreas, about 5.8 miles west. There are a series of folds in the marine terraces and one of the folds has been mapped as a compressional fault between Hare Creek and the Noyo River near PM 60.1. This is not an active fault, but rather a mapped remnant of previous tectonic activity. The potential for surface fault rupture does not exist.

#### Liquefaction

Based on the depth of groundwater and the subsurface soil/rock conditions in the nearest borings, the potential for liquefaction does not exist.

#### **Analyses and Design**

#### Project Design Information

As stated in the Project Description section, Table 1 provides a summary of the retaining walls. RW-1N is a Standard Plan Retaining Wall, Type 6A (Case 2), with a maximum height of 6 feet. Based on the project plans, the backfill slope angle is 2H:1V. RW-2S is a Standard Plan Retaining Wall, Type 6B (Case 1), with a maximum height of 4 feet.

Standard Plan Earth Retaining Systems (ERS) are designed based on a horizontal seismic acceleration coefficient of 0.2g, corresponding to a HPGA of 0.6g. The proposed retaining wall sites have an HPGA greater than 0.6g. A Standard Plan ERS can be used in areas with a HPGA greater than 0.6g if the resulting permanent seismic displacement is acceptable for the project. It is the District's responsibility to determine how much permanent seismic displacement is acceptable for the subject project.

#### Soil/Rock Engineering Properties

The soil and rock engineering properties were estimated from the nearest borings and are summarized in Table 3A and Table 3B.

Table 3A: RW-1N Soil Engineering Properties

	Lover			Interpre	eted Soil Eng Properties	•
Layer No.	Layer Boundaries <sup>1</sup> , Depth (feet)	General Soil Description	SPT N Value	Effective Unit Weight (γ'), pcf	Apparent Cohesion (C), psf	Effective Friction Angle (Φ), degrees
1	Ground Surface to 6	Dune Sand	13-27	120	0	32
2	6 to 8	Decomposed Sandstone	19-22	125	0	36
3	8 to 11	Decomposed Sandstone	19-22	63	0	36
4	Below 11	Sandstone	>50	68	0	40

<sup>1. 0-</sup>foot depth is top of footing.

Table 3B: RW-2S Soil Engineering Properties

	Layer			Interpre	eted Soil Eng Properties	
Layer No.	Boundaries <sup>1</sup> , Depth (feet)	General Soil Description	SPT N Value	Effective Unit Weight (γ'), pcf	Apparent Cohesion (C), psf	Effective Friction Angle (Φ), degrees
1	Ground Surface to 1	Structure Backfill	N/A	120	0	34
2	1 to 11	Loose Clayey Sand	6	120	0	28
3	11 to 31	Decomposed Sandstone	18-47	125	0	36

<sup>1. 0-</sup>foot depth is top of footing.

#### Geotechnical Model and Analyses

The footings for RW-1N and RW-2S will be generally founded in medium dense to dense sands and loose sand, respectively. The factored bearing resistance of the soil will exceed the minimum bearing stresses shown on the Standard Plans.

Since the site HPGA is greater than 0.6g, permanent seismic displacement analyses were performed. The Bray et al. (2010) and Bray and Travasarou (2009) methods were used. Based on the analyses, a permanent seismic displacement of 6 inches was estimated.

Global slope stability analyses were performed for Service and Extreme Event Limit States. A horizontal seismic acceleration coefficient of 1/3HPGA (0.22g) was used for the extreme event. Two-dimensional slope stability analyses were performed using the

DUNG SY October 31, 2022 Page 7 Geotechnical Design Report Fort Bragg ADA RW-1N and RW-2S 01-0B220 / 0112000110

program Slide2 by Rocscience. The factors of safety exceed 1.5 (resistance factor = 0.65) and 1.1 (resistance factor = 0.9) for service and extreme events, respectively.

#### Recommendations

#### Standard Plan Earth Retaining System

A Standard Plan Retaining Wall, Type 6A (case 2) and 6B (case 1), are acceptable from a geotechnical standpoint. The District shall verify if 6 inches of permanent seismic displacement is acceptable for the project.

Site-specific borings were not performed for the retaining walls; the nearest borings were used for design. The subsurface soils may vary from those disclosed in the nearest borings. Therefore, the footing excavations for RW-1N and RW-2S are to be inspected and approved by the Office of Geotechnical Design West (OGDW), Branch A. The inspections are to be made after the excavation has been completed to the bottom of footing elevations and prior to placing rebar or concrete in the excavations. The contractor is to allow seven working days for the inspection of each footing excavation to be completed. The Structures Representative is to provide OGDW, Branch A, one-week notification prior to beginning the seven-day contractor waiting period.

Site-specific corrosion testing was not performed. It should be assumed that the on-site soils are corrosive.

#### **Notes for Specifications**

SSP 90-1.02H – Concrete in Direct Contact with a Corrosive Environment

Concrete in direct contact with native soil should be considered in a corrosive environment.

Questions relating to this report should be directed to Nick Briffa at (213) 604-4261 or Branch Chief John Moore at (510) 622-8742.

NICK BRIFFA

Transportation Engineer

Office of Geotechnical Design West

Branch A

JOHN MOORE

Chief, Branch A

Office of Geotechnical Design West

CHRIS RISDEN OF Chief, Branch B

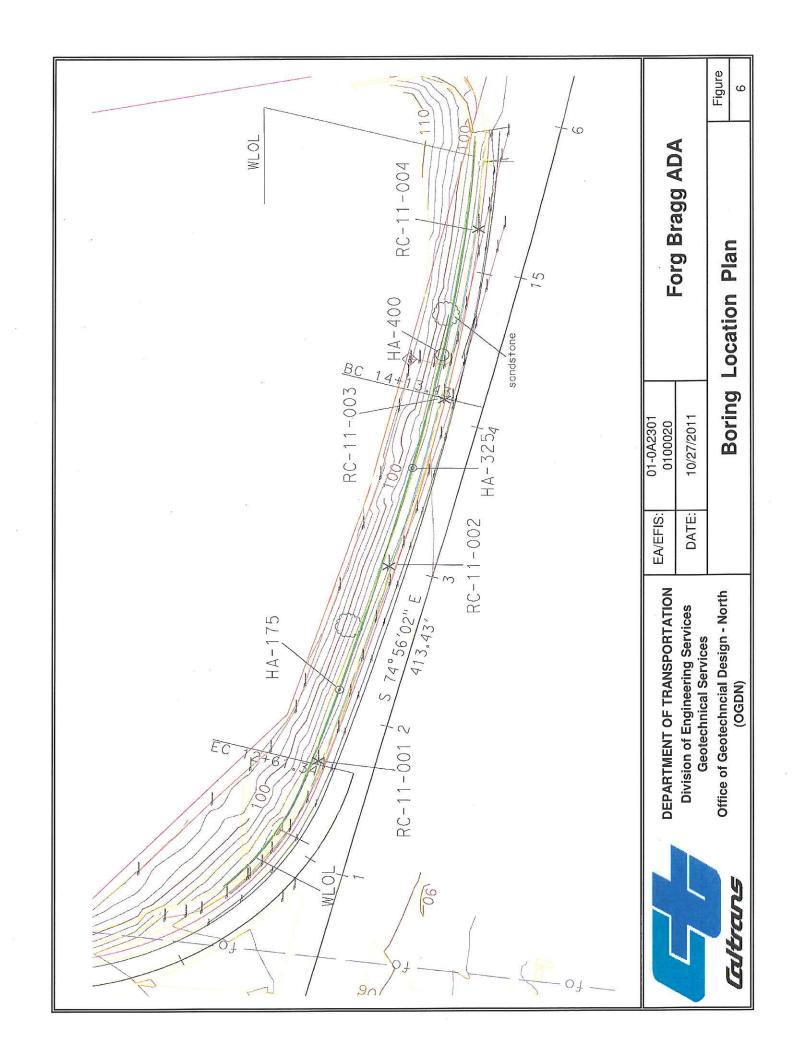
Office of Geotechnical Design West

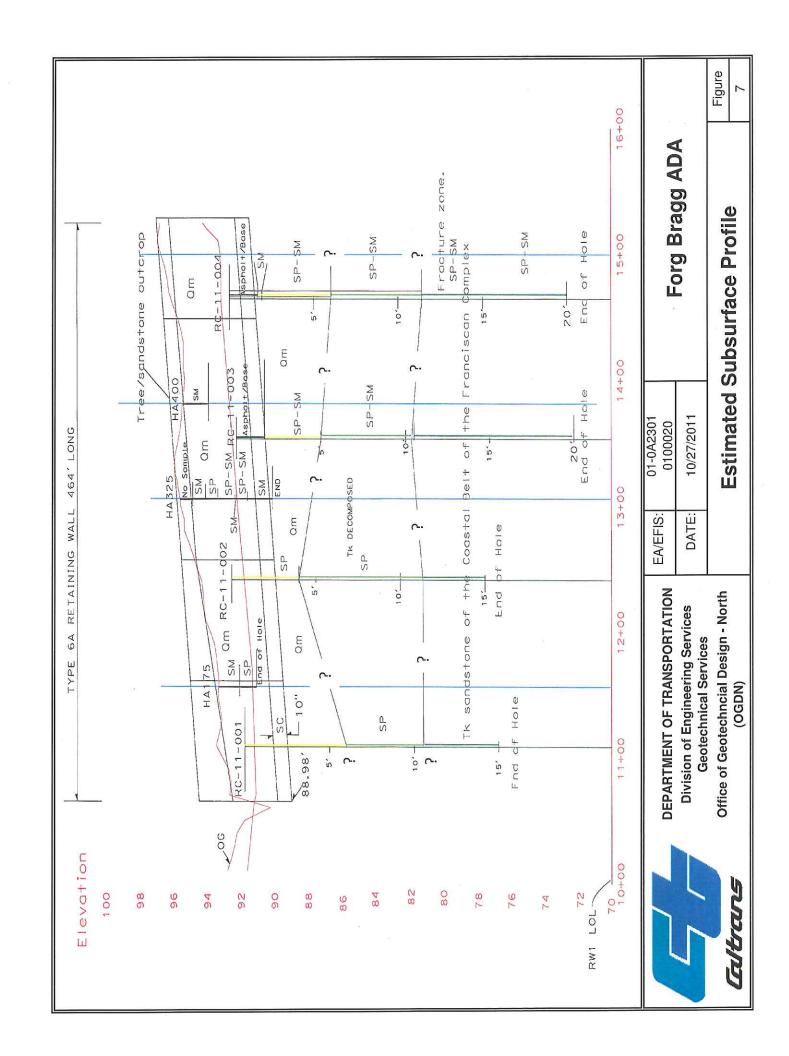
#### **Attachment**

Appendix A Pertinent Subsurface Investigations

c: Robert King, Project Manager, District 3
Andre Guimaraes, District Materials Engineer, District 1

# APPENDIX A PERTINENT SUBSURFACE INVESTIGATIONS





TL-1271a (REV. 01/31/00)

BORING NUMBER DATE
HA-175 08/25/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Wall Station: 11+57
TOP HOLE ELEVATION

92.84

**BOTTOM HOLE ELEVATION** 

NOTES		EQUIPTME	ENT	CHC NUMBER
Fort Bragg	PROJECT NAME g ADA	E	A 01-0A2310//EFIS	EA NUMBER S 0100020260
01	MEN	20	R0.0/R0.1	
DIST.	CO.	RTE.	P.M. (K.P.)	BRIDGE #

SUMMARY

HA-107 OWBC-11-001	SITE LOCATION MAP (Inc. North Arrow & Benchmark Datum)
POLE  HA-175 RCE 11 MOOZ PE  5 742 56'02" E28' From on  413.43'  3	HA-107 O RC-11-001 POLE HA-175 RCE11MOORE

SW .	DATE
GWS	DATE
CASING SIZE	CASING DEPTH
CASING SIZE	CASING DEPTH
SLURRY TYPE	

DEMARKS	FI	ELD 1	ESTI	NG			DESCRIPTION
REMARKS (Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH (inches)	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
Hole advanced with a					1		
3.25" sand auger					2		
a .					3		Silty SAND (SM); dusky red; dry to moist; mostly fine SAND; little to some fines; few fine
					5	-	GRAVEL, angular to subangular; weak cementation; roots 0-9"
					7		commentation, roots v
					8		
SV					9		
					10		trace coarse to fine GRAVEL, angular;
*					11		beach/dune sand present
					12		
	¥				13		beach/dune sand present
					582.63	;: 1:: 	
					15		
					16		
					17	-	Poorly graded SAND (SP); dry to moist; light
					18		brownish gray; mostly fine SAND (dune sand); weak cementation
					19	-	weak contentation

TL-1271b (REV. 01/31/00) BORING NUMBER HA-175	DATE 08/25/20	11		0	IST. l			CO. MEN	RTE. 20	P.M. (K.P.) R0.0/R0.1	
OCATION (STA/OFFSET or 92.84'	NORTHING/EASTIN	G)			OP HC 92.84		EVAT	VATION BRIDGE # EA NUMBE EA 01-0A2310//EFIS 010002026			
		FI	ELD 1	TESTI	NG			DESCRIPTION	-	x	
REMARK (Tool Sizes/Type - Ro (Hole Condition – Caving, S Circulation, Drill Rig reactions – slov skipping, block	ds & Bits, etc) Squeezing, Loss of etc. wing, chattering,	SAMPLE #	SPT (N) Recovery %				GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, void slaking, odor, other characteristics)			
						22				, (ab)	
		i.				23			AND with GRAV noist; mostly SAI		
		-		1		24			lar; little to some		
		_				25		from coarse to f	ine, includes igne		
	9					26 27		subangular; wea	k cementation.		
						28					
						29		,			
						30					
					_	31					
						32	-				
						33				<u>#</u>	
						34	-				
						35					
						36	-				
	"		_			37					
						38	-				
						39					
						40	-				
						42					
						43	-				
						44					
						45					
						46					
						47					
						48					
						49		10			
				2		50	-				
						51					
			1			52	1	10			

TL-1271a (REV. 01/31/00)

AUGER HOLE NUMBER DATE
HA-325 08/24/25/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Wall Station: 13+6.28

TOP HOLE ELEVATION

**BOTTOM HOLE ELEVATION** 

95.6'

 01
 MEN
 20
 R0.0/R0.1

 BRIDGE OR PROJECT NAME
 EA NUMBER

 Fort Bragg ADA
 EA 01-0A2310//EFIS 0100020260

RTE.

CREW EQUIPTMENT

DIST.

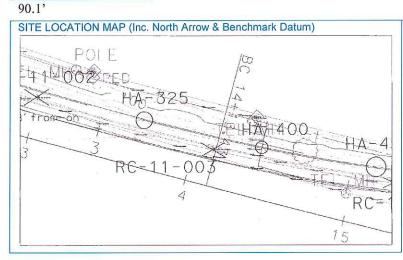
CHC NUMBER

BRIDGE#

Beach/dune sand 91' - 93' elevation

CO.

SUMMARY: Beach/dune sand 2.25-4 ft depth; igneous clasts in 48"-60"



GW .	DATE
GWS	DATE
CASING SIZE	CASING DEPTH
CASING SIZE	CASING DEPTH
SLURRY TYPE	

P.M. (K.P.)

REMARKS	FI	ELD 1	FESTI	NG			DESCRIPTION Sail Clearification (group page group gymbol
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition – Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions – slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	ELEVATION	DEPTH (feet)	DEPTH (inches)	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
Hole advanced with a					1		
3.25' sand auger					2		
					3		
					4		
					5		0-9" No Samples
					6		*
					7		
					8		
9					9		
					10	331	
					11		
94.6' at bottom of this cell			94	1	12		
					13		Silty SAND (SM); pinkish gray; dry; mostly SAND, fine; little to few fines; little to few GRAVEL, fine,
					14		subangular; weak cementation.
				1.25	15		•
9					16		
					17		
94.1' at bottom of this cell			93.5	1.5	18		
					19		
					20		Poorly graded SAND (SP)
				1.25			Commenter that the comment of the co

TL-1271b (REV. 01/31/00)

BORING NUMBER DATE DIST. CO. RTE. P.M. (K.P.) R0.0/R0.1 HA-325 08/24/25/2011 01 MEN 20

LOCATION (STA/OFFSET or NORTHING/EASTING)
Wall Station: 13+6.28

BRIDGE #

EA NUMBER

TOP HOLE ELEVATION

Wall Station: 13+6.28			0	95.6'			EA 01-0A2310//EFIS 0100020260
	FI	ELD 1	ESTI	NG			DESCRIPTION
REMARKS (Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	ELEVATION	DEPTH (feet)	DEPTH (inches)	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, q <sub>u</sub> , s <sub>u</sub> , Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
					22	-	
93.6' at bottom of this cell			93	_	23		Poorly graded SAND (SP); reddish brown; dry; mostly
93.0 at bottom of this cen			73	2	24	-	SAND, fine; few GRAVEL, fine, angular to subangular;
					25		weak cementation
х				100000	26	-	
				2.25	27		D. J. and J. CAND. with CH. T. (CD. CM.). doubt its dilich
					28	-	Poorly graded SAND with SILT (SP-SM); dark reddish brown; moist; mostly SAND, coarse to fine (beach/dune
			92.5		29		sand included), subrounded to subangular; few to little
93.1' at bottom of this cell			92,3	2.5	30		GRAVEL, coarse to fine; subangular to angular; weak
	31 cementation.	Contentation.					
					32		1 1/1
				2.75	33		beach/dune sand
					34		
					35		
93.1' at bottom of this cell			92	3	36		
					37		
e.					38		
				3.25	39		
					40		Silty SAND with GRAVEL (SM); reddish brown; moist; mostly SAND, from coarse to fine, angular; little fines; little GRAVEL, coarse to fine,
					41		angular, intensely weathered rock; weak cementation.
92.1' at bottom of this cell			91.5	3.5	42	171	
					43		
v					44		Poorly graded SAND with SILT (SP-SM); very pale
				3.75	45		brown; moist; mostly SAND, fine, rounded quartz
				190000	18/A-2000		beach/dune sand; few to little fines; trace Gravel, fine (soft clumps of silty sand); weak cementation
					46		clumps of sitty said), weak comentation
91.6' at bottom of this cell			91	4	47 48		a .
71.0 at obttom of this con			7.	4			
					49		
				117000000	50		Silty SAND (SM); brownish yellow to reddish brown
				4.25	51		(redder below 48"); moist; mostly SAND, from coarse to
					52		fine; little to some fines, includes coarse white fragments of igneous rocks; few-trace GRAVEL, fine, subangular
					53	1 :41	
91.1' at bottom of this cell			90.5	4.5	33		(including hard igneous rocks); weak cementation

TL-1271b (REV. 01/31/00)

LOCATION (STA/OFFSET or NORTHING/EASTING)TOP HOLE ELEVATIONBRIDGE #EA NUMBERWall Station: 13+6.2895.6'EA 01-0A2310//EFIS 0100020260

				93.0			EA 01-0A2310//EF13 0100020200
REMARKS	F	IELD .	TESTI	NG			DESCRIPTION
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc.  Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	ELEVATION	DEPTH (feet)	DEPTH (inches)	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
					55		
					56		
				4.75	57		
×					58		
т.					59		
90.6' at bottom of this cell			90	5	60		few GRAVEL, coarse to fine, angular (very soft sandstor
¥ .					61		clasts-weathered bedrock?)
g g					62		
				5.25	63		
					64		increase in fines to "some fines"
							conscious streethine street substituted aboves. Substituted statements.
90.1' at bottom of this cell			89.5	5.5	65 66	-	*
				3.3			End of auger hole at 66"
					67		
					68		
					69		
			-		70		
					71		
					72	-	
					73		
					74		
					75		"
					76		
					77		
					78	18	
					79		
					80		
					81		
		2:			82		
					83		- W
					84		
					85		a a
					86		
					87		

TL-1271a (REV. 01/31/00)

BORING NUMBER DATE HA-400 08/24/2011

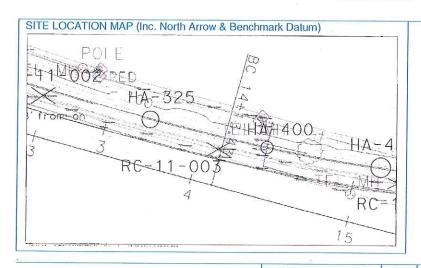
LOCATION (STA/OFFSET or NORTHING/EASTING)

Wall Station: 13+82

TOP HOLE ELEVATION 95.43

DIST.	CO.	RTE.	P.M. (K.P.)	BRIDGE #		
01	MEN	20	R0.0/R0.1			
BRIDGE OF	R PROJECT NAME			EA NUMBER		
Fort Bragg ADA		E	A 01-0A2310//EFI	0//EFIS 0100020		
CREW		EQUIPTME	ENT	CHC NUMBER		

HAMMER ID#



GW	DATE
GWS	DATE
CASING SIZE	CASING DEPTH
CASING SIZE	CASING DEPTH
SLURRY TYPE	
SUBFACE CONDITION	ONS (Slope, Water, Vegetation, etc)

REMARKS	FIELD TESTING				8		DESCRIPTION Sell Clearification (group ages and to the			
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition – Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions – slowing, chatţering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, q <sub>u</sub> , s <sub>u</sub> , Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)			
Hole advanced with a					1	111	Silty SAND with GRAVEL (SM); loose;			
3.25" sand auger					2		brownish yellow; moist; mostly SAND, fine;			
2					3		little fines; little fine to coarse GRAVEL;			
					4		subangular. Gravel consists of soft fragments of			
4					5		intensely weathered fine sandstone.			
					6					
					7		8			
					8		φ.			
			- 4		9					
					10		at the state of th			
					11	-11				
					12					
					13					
					14	111				
		22			15	111				
				1	16					
					17					
					18	191				
					19	: EU				
- 3										
					20	-				
				til	21					

TL-1271a (REV. 01/31/00) BORING NUMBER DATE RC-11-001 09/07/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 11+67, 31 L

TOP HOLE ELEVATION

91.78

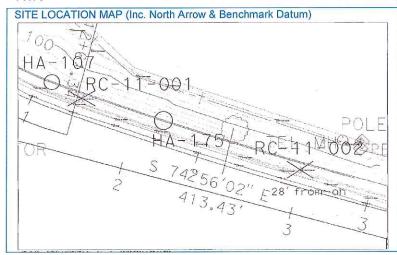
**BOTTOM HOLE ELEVATION** 

76.78

DIST.	CO.	RTE.	P.M. (K.P.)				
01	MEN	20	R0.0/R0.1				
PROJECT				EA NUMBER			
Fort Bragg ADA  CREW  Eureka Drill Crew		EA 01-0A2310//EFIS 010002020					
		EQUIPTME	ENT	CHC NUMBER			
		Acker		1974			

HAMMER

Automatic, ER=80% (Calibrated 04/19/2011)



LOGGER D. McGuire	
GW	DATE
GW	DATE
CASING SIZE	CASING DEPTH
94 mm	10'
CASING SIZE	CASING DEPTH
SLURRY TYPE	
None	Drilled with Water
SURFACE CONDITION	ONS (Slope, Water, Vegetation, etc)
	t sun in later morning; dry; drilled into

REMARKS	F	IELD 7	TEST	ING		9	DESCRIPTION
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc.  Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, q <sub>u</sub> , s <sub>u</sub> , Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)
Mud rotary punch core, 4.75" finger bit		4			1		Clayey SAND (SC); medium dense; reddish brown;
to 10.6'. Drilled dry to 2'.		5			2		moist; mostly SAND, fine; little fines; weak cementation to 3". [Qm]
Corrected N: 13 x 1.33=17.3, medium dense		8	13	1	3		moderate cementation from 3'to 5'
					5		brownish yellow from 3' to 7'.
Corrected N: 22 x 1.33=29, medium dense		18			6		fewer fines; weak cementation; becoming decomposed sandstone
		9			7	1,1,1	SEDIMENTARY ROCK (Sandstone); brownish yellow;
		13	22		8		intensely weathered to decomposed; (Poorly graded SAND (SP); medium dense; moist; mostly SAND, from coarse to
					9		fine; little fines; few GRAVEL, from coarse to fine, angular
E.					10		weak cementation). [DECOMPOSED BEDROCK, Tk]
Refusal at 10.6' 81.1' elevation)		41			11		SEDIMENTARY ROCK (Sandstone); massive; yellowish
3 ¾"diamond core bit from 10.6' to 15'.		65/1.5	R		12		brown; intensely weathered; moderately hard; very intensely fractured. [BEDROCK, Tk]
	4				13		Hactured. [BEDROCK, 1k]
					14		
End of hole at 15' (Elevation 76.78').					15		
Perforated 0- 10'. Bentonite below 10'.					16		
One bag of sand					17		
					18		
*			84		19		
					20		
					21		

TL-1271a (REV. 01/31/00)

BORING NUMBER DATE RC-11-002 09/07/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 13+00, 25.3 L

TOP HOLE ELEVATION

92.54

BOTTOM HOLE ELEVATION

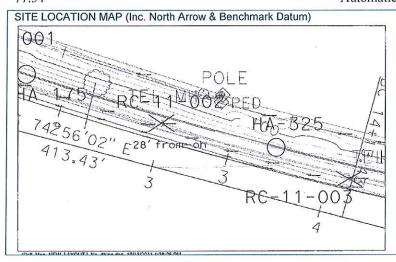
77.54

DIST.	CO.	RTE.	P.M. (K.P.)	
01	MEN	20	R0.0/R0.1	
PROJECT				EA NUMBER
Fort Bragg ADA		Е	A 01-0A2310//EFI	S 0100020260
CREW		EQUIPTMI	ENT	CHC NUMBER
Eureka Drill Crew		Acker		1974

HAMMER

Automatic, ER=80% (Calibrated 04/19/2011)

N



GW	DATE
9.3' bgs	9/8/2011
GW	DATE
CASING SIZE	CASING DEPTH
94 mm	15'
CASING SIZE	CASING DEPTH
SLURRY TYPE	
None	Drilled with Water
SURFACE CONDITI	ONS (Slope, Water, Vegetation, etc)
Sunny side of a for	g bank, surface dry, drilled into soil
adiacent to adiacen	nt to edge of pavement,

IDER Man NITH LEVOLIT I No dales das 50/12/2011 1/38/96 DM				***************************************		L	
REMARKS	F	IELD 7	rest	ING		ပ္	DESCRIPTION
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition - Caving, Squeezing, Loss of Circulation, etc.  Drill Rig reactions - slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, qu, su, Other characteristics)  Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor other characteristics)
Mud rotary punch core, 4.5" finger bit to		4			1		Poorly graded SAND (SP); dense; reddish brown; moist; mostly SAND, fine to coarse; little fines; weak cementation to (0" to 6").
10.75'. Drilled dry to 2'.		6			2		[Qm]
Corrected N: 27x 1.33=36 (dense due to		21	27		3		Brownish yellow; trace to few GRAVEL, coarse; subangular (6" t 1.5').
a fragment of coarse gravel)					4		
	9				5		Poorly graded SAND with SILT and GRAVEL (SP-SM); dense to medium dense; brownish yellow; moist; mostly SAND, from
Corrected N: 19x 1.33=25.3 (medium		13			6	- 14:13:	coarse to fine; little GRAVEL, fine, from angular to subrounded;
lense)		7			7		cementation from weak to moderate (1.5'-5').
		12	19		8		
					9		SEDIMENTARY ROCK (Sandstone); brownish yellow; intensely weathered to decomposed; (Poorly graded SAND (SP); medium
					10		dense; moist; mostly SAND, fine; little fines; moderate
Refusal at 11.3' (81.24')		14			11		cementation). [DECOMPOSED BEDROCK, Tk]
3 ¾"diamond core bit from 11.3' to 15'.		50/5.5	¥		12		ODDIN (ENVELDY DOCK (O. ) L. ) See les del servici
*		50/3.5	100/9		13		SEDIMENTARY ROCK (Sandstone); massive; dark grayish brown; intensely weathered; moderately hard; very intensely
8					14		fractured. [BEDROCK, Tk]
End of hole at 15' (77.54' elevation).					15		
Casing perforated 5' to 15'.					16	-	***
Two bags of sand and bentonite.					17		
					18		
					19		ė
					20		
					0.1	1	

TL-1271a (REV. 01/31/00)

BORING NUMBER DATE RC-11-003 09/08/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 14+13, 23 L;

TOP HOLE ELEVATION

92.24

**BOTTOM HOLE ELEVATION** 

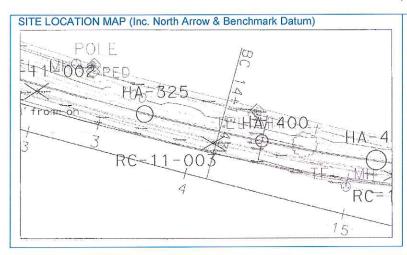
72.24

DIST.	CO.	RTE.	P.M. (K.P.)
01	MEN	20	R0.0/R0.1
PROJECT			EA NUMBE
Fort Bragg ADA		E	A 01-0A2310//EFIS 0100020260
CREW	225	EQUIPTME	ENT CHC NUMB
Eureka Drill Crew		Acker	1974

HAMMER

Automatic, ER=80% (Calibrated on 04/19/2011)

N



W	DATE
W	DATE
ASING SIZE	CASING DEPTH
4 mm	20'
ASING SIZE	CASING DEPTH
LURRY TYPE	
one	Drilled with Water
JRFACE CONDITION	ONS (Slope, Water, Vegetation, etc)

REMARKS	F	IELD 7		Ö			
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition – Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions – slowing, chattering, skipping blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	GRAPHIC LOG	Sockho
Mud rotary punch core, 4 ¾" finger bit					1		
to 10.5'. Dry SPT 0-1.5'.					2		
		12			3		
		27			4		
18"-36" very dense, N>50		31	58		5		
a a		33			6		=
Very dense, N>50		60/6			7		
		29	89/12		8		
					9		
					10		
Refusal at 10.5' (81.74' elevation).		50/5.5	R		11		
3 ¾"diamond core bit from 10.5' to 20'.					12		
					13		
18					14		
8	ĺ				15		
					16		
					17		
End of hole at 20' (elevation 72.24')					18		
Casing perforated 10' to 20'.					19		
Two bags of sand; bentonite to seal hole.					20		

#### DESCRIPTION

Soil Classification (group name, group symbol, consistency/relative density, color, moisture, particle size, gradation, plasticity, structure, cementation, organics, fill, q<sub>u</sub>, s<sub>u</sub>, Other characteristics)

Rock Classification (rock name, color, degree of weathering, relative hardness, bedding, discontinuity characteristics, voids, slaking, odor, other characteristics)

ASPHALT and road base.

Poorly graded SAND with SILT (SP-SM); very dense; brownish yellow to yellowish red; moist; mostly SAND, fine; few to little fines; from moderate to weak cementation. [Qm]

SEDIMENTARY ROCK (Sandstone); brownish yellow; very intensely weathered to decomposed; (Poorly graded SAND with SILT and GRAVEL (SP-SM); very dense; moist; mostly SAND, fine; few to little fines; from moderate to weak cementation.). [DECOMPOSED BEDROCK, Tk]

SEDIMENTARY ROCK (fine-grained Sandstone); massive; reddish brown; intensely weathered; moderately soft; very intensely fractured; fracture zone. [BEDROCK, Tk]

TL-1271a (REV. 01/31/00)

**BORING NUMBER** DATE RC-11-004 09/08/2011

LOCATION (STA/OFFSET or NORTHING/EASTING)

Roadway Station: 15+25, 31.3 L

TOP HOLE ELEVATION

92.64

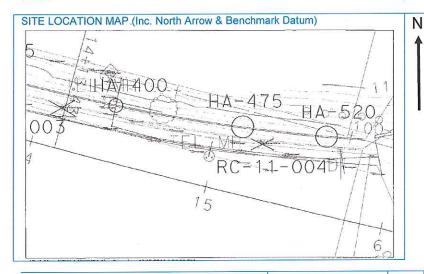
**BOTTOM HOLE ELEVATION** 

72.64

DIST. CO.		RTE.	P.M. (K.P.)	(.P.)		
01	MEN	20	R0.0/R0.1			
PROJECT				EA NUMBER		
Fort Bragg ADA  CREW Eureka Drill Crew		E.	EA 01-0A2310//EFIS 0100020260			
		EQUIPTME	NT	CHC NUMBER		
		Acker		1974		

Automatic, ER=80% (Calibrated 04/19/2011)

HAMMER



DATE  CASING SIZE CASING DEPTH					
CASING SIZE CASING DEPTH					
94 mm 20°	20'				
CASING SIZE CASING DEPTH	CASING DEPTH				
SLURRY TYPE					
None Drilled with Water					
SURFACE CONDITIONS (Slope, Water, Vegetat	ion, etc)				

REMARKS	FIELD TESTING					90	DESCRIPTION
(Tool Sizes/Type - Rods & Bits, etc) (Hole Condition – Caving, Squeezing, Loss of Circulation, etc. Drill Rig reactions – slowing, chattering, skipping, blocking off)	SAMPLE #	BLOWS PER 6"	SPT (N)	Recovery %	DEPTH	SRAPHIC L	Soil Classification (group density, color, moisture, p cementation, organics, fill Rock Classification (rock hardness, bedding, disco other characteristics)
Mud rotary punch core; 4 ¾" finger bit.					1		ASPHALT and road ba
		10			2		Poorly graded SAND w
Corrected N (20"-38"): 15x 1.33=20		7			3		brown; moist; mostly Saccementation (1.7'-4.3')
Medium dense		8	15		4		very dense; brownish ye to fine; (4.3'-5.3'). [Qm
					5		
		13			6		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
Very dense, N>50		20			7	- 11	SEDIMENTARY ROC
		37	57		8		weathered to decompo
					9		SM); very dense; moist; moderate cementation. (
					10		BEDROCK, Tk]
Refusal at 11.4' (81.2' elevation)		22			11		]
3 ¾"diamond core bit from 11.4' to 20'.	-	37			12		SEDIMENTARY ROO
		60/5	97/11		13		weathered to decompose
					14		SM); very dense; moist; coarse; few to little fine
					15		Tk].
18' drill rate increased through soft material					16		* ,
and black organic film appeared in mud pit.	1				17		fracture zone 18'-20'.
End of hole at 20'(elevation 72.64).	+				18		
Casing perforated 10' to 20'.					19		gray at 19'-20'.
Two bags of sand; bentonite plug).					20		-

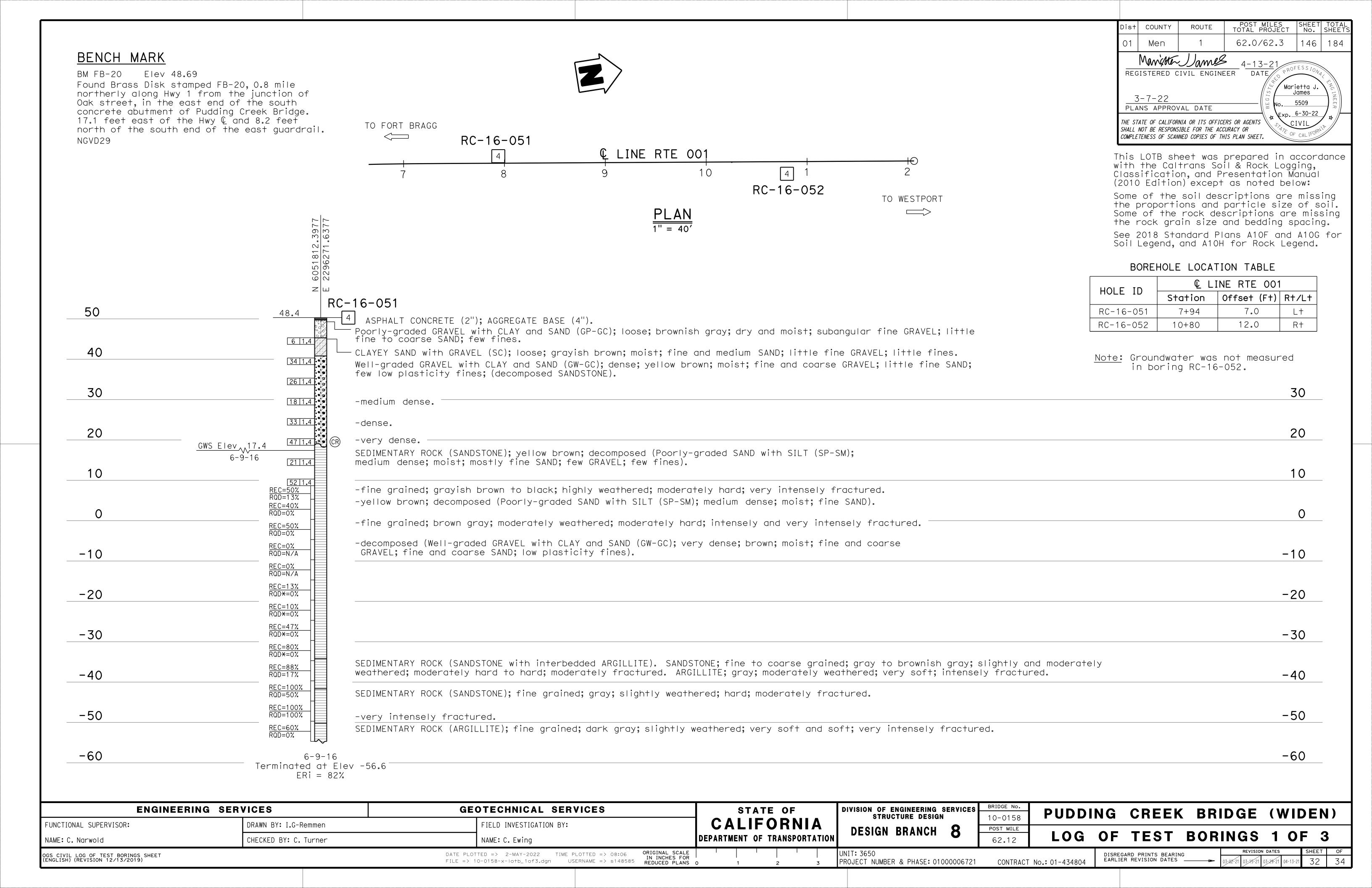
o name, group symbol, consistency/relative particle size, gradation, plasticity, structure, ill, qu, su, Other characteristics) name, color, degree of weathering, relative ontinuity characteristics, voids, slaking, odor,

with SILT (SP-SM); medium dense; reddish SAND, fine; few to little fines; moderate ) [Qm}

vellow; few to little GRAVEL, from coarse

CK (Sandstone); reddish brown; intensely sed; (Poorly graded SAND with SILT (SPt; mostly SAND, fine; few to little fines; (5.3'-11.4'). [DECOMPOSED

CK (Sandstone); reddish brown; intensely sed; (Poorly graded SAND with SILT (SPt; mostly SAND, mostly fine but includes es; moderate cementation) [BEDROCK,



From: King, Robert W@DOT

To: Umbertis, Stephen@DOT; Arreola, Ash@DOT; Stillmunkes, Keith P@DOT; Briffa, Nick@DOT; Meyer, Jason

J@DOT; Gurewitz, Heather; Ranu Aggarwal

Cc: Sy, Dung@DOT; Moore, J C@DOT

Subject: RE: review of Standard Plan wall design

Date: Tuesday, November 15, 2022 2:58:23 PM

Attachments: Geotech Memo Revised 9-12-22.pdf

01-0B220 MEN101 PM59.8-62.1 FortBraggADA GDR 2022.10.31.pdf

**[EXTERNAL EMAIL]** DO NOT CLICK links or attachments unless you know the content is safe. Be aware that the sending address can be faked or manipulated.

Hi Ranu,

Attached are the Geotech Memo and the Geotechnical Design Report.

The District confirms that 6" of permanent seismic displacement is acceptable for the project.

6" of seismic displacement would only occur during an earthquake of magnitude M7.57.

In addition, this is a landscape retaining wall and has historically performed well during seismic events. In the event of any damage to the retaining wall, Caltrans Maintenance would be dispatched immediately to cleanup any debris and Caltrans would immediately make plans to repair the retaining wall.

Thanks

Robert King, PE
Project Manager
Caltrans - District 1
Cell (707) 296-5573

https://cadot.webex.com/meet/robert.king

-----Original Appointment-----

From: Umbertis, Stephen@DOT <Stephen.Umbertis@dot.ca.gov>

Sent: Tuesday, November 15, 2022 12:40 PM

To: Umbertis, Stephen@DOT; Arreola, Ash@DOT; Stillmunkes, Keith P@DOT; Briffa, Nick@DOT;

Meyer, Jason J@DOT; Gurewitz, Heather; Ranu Aggarwal **Cc:** King, Robert W@DOT; Sy, Dung@DOT; Moore, J C@DOT

**Subject:** review of Standard Plan wall design

When: Tuesday, November 15, 2022 2:00 PM-2:30 PM (UTC-08:00) Pacific Time (US & Canada).

Where: webex

Meeting with City of Fort Bragg Staff and consultant to discuss the use of the Standard Wall Plan approved in the attached email.

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